

School of Engineering And Applied Sciences Building

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Structural Option

Miami University
Oxford, OH





Building Background

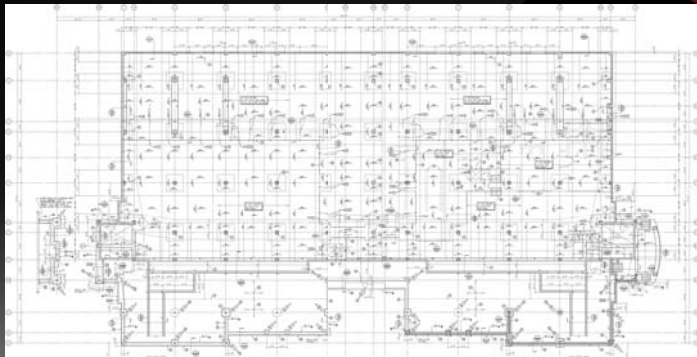
- Connected to existing Benton Hall via skywalk
- Size: 103,154 SF above grade on 4 levels
82,661 SF below grade parking on 3 levels
- Cost: \$23,651,159
- Constructed: Oct. 2004 – Jan. 2007
- Delivery Method: Design-Bid-Build
- General Contractor: Monarch Construction
- Architect: Burt Hill Kosar Rittleman Associates
- Structural Engineer: THP Limited

Presentation Outline

- Introduction
 - *Building Background*
 - Project Goals
- Structural Depth
- Building Enclosures Breadth
- Construction Management Breadth
- Conclusions

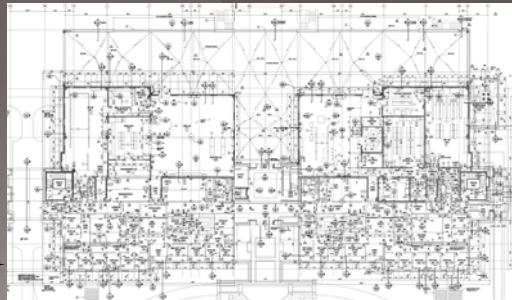


Ground Floor Framing Plan



Existing Conditions

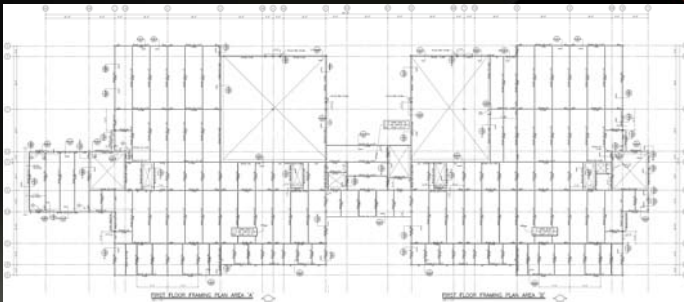
- Substructure
- Ground Floor and Garage
 - 2-way C.I.P. slab with drop panels



Presentation Outline

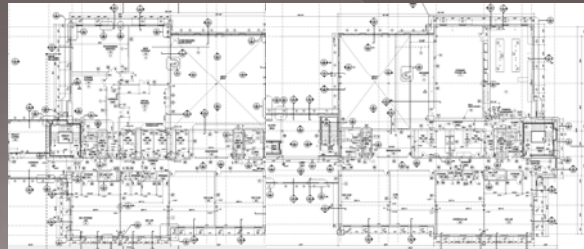
- Introduction
- Structural Depth
 - Existing Conditions*
 - Proposed Redesign
- Building Enclosures Breadth
- Construction Management Breadth
- Conclusions

First Floor Framing Plan



Existing Conditions

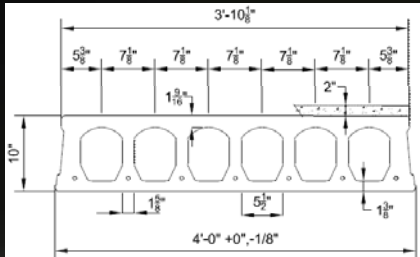
- Superstructure
 - 1st, 2nd, Mechanical, and Roof Levels
 - 3½" Composite slab on 3" composite deck on steel frame structure



Presentation Outline

- Introduction
- Structural Depth
 - *Existing Conditions*
 - Proposed Redesign
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Hollowcore Floor Planks



10" Hollowcore Plank with 2" Concrete Topping
ECHO by Nitterhouse Concrete Products, Inc.

PHYSICAL PROPERTIES Composite Section	
$A_c = 327 \text{ in}^2$	Precast $S_w = 824 \text{ in}^3$
$I_c = 5102 \text{ in}^4$	Topping $S_w = 1242 \text{ in}^3$
$Y_c = 6.19 \text{ in.}$	Precast $S_w = 1340 \text{ in}^3$
$Y_t = 3.81 \text{ in.}$	Wt = 272 PLF
	Wt = 68.00 PSF

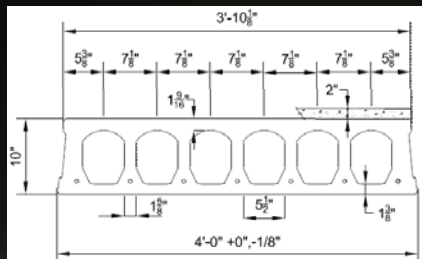
Proposed Redesign

- Goals and Design Constraints
 - Accelerated construction schedule
 - Decrease or maintain cost
 - Do not change architecture
 - Maintain floor-to-ceiling and total heights
- Method
 - Prefabricated structure
 - Precast concrete hollowcore floor planks
 - Supported on similar steel frame

Presentation Outline

- Introduction
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- Building Enclosures Breadth
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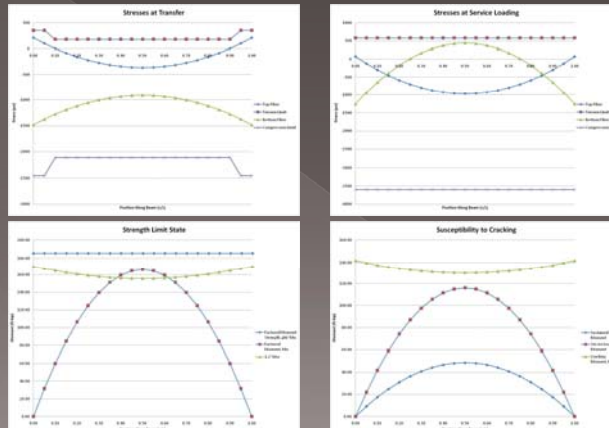
Hollowcore Floor Planks



10" Hollowcore Plank with 2" Concrete Topping
ECHO by Nitterhouse Concrete Products, Inc.

PHYSICAL PROPERTIES Composite Section	
$A_c = 327 \text{ in}^2$	Precast $S_{xc} = 824 \text{ in}^3$
$I_c = 5102 \text{ in}^4$	Topping $S_{xt} = 1242 \text{ in}^3$
$Y_{c-x} = 6.19 \text{ in.}$	Precast $S_{xc} = 1340 \text{ in}^3$
$Y_{c-y} = 3.81 \text{ in.}$	Wt = 272 PLF
	Wt = 68.00 PSF

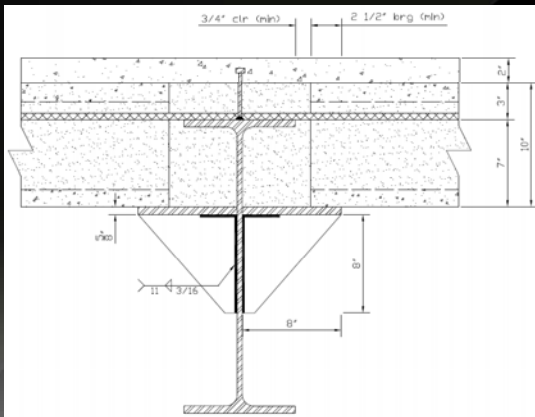
Hollowcore Floor Planks



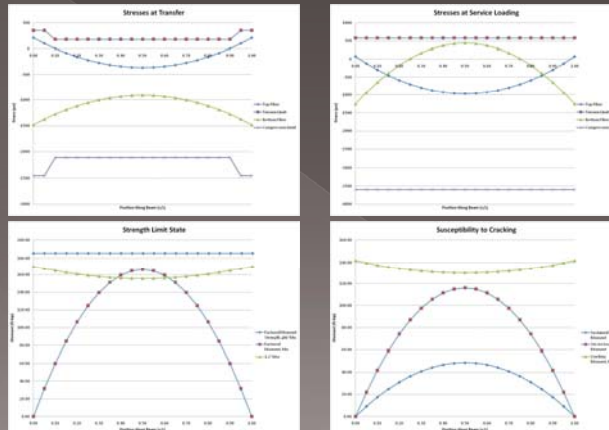
Presentation Outline

- Introduction
- Structural Depth
 - Existing Conditions
 - *Proposed Redesign*
- Building Enclosures Breadth
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Support System



Hollowcore Floor Planks



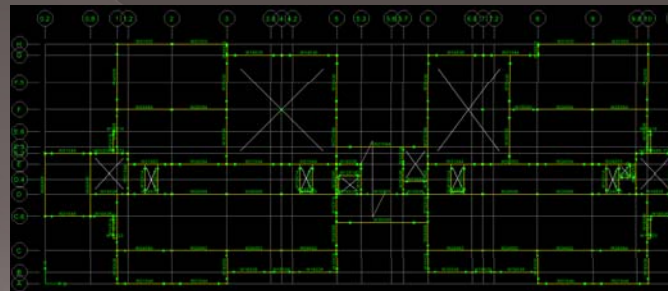
Presentation Outline

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Seismic Loads

Seismic Design Summary			
Design Parameter	Symbol	Value	ASCE 7-05 Reference
Occupancy category		III	Table 1.1
Site classification		C	Table 20.3-1
Seismic Design Category	SDC	B	Tables 11.6-1 & 2
Seismic importance factor	I	1.25	Table 11.5-1
Short period spectral response	S_s	0.171g	Section 11.4.1
Acceleration-based Site coefficient	F_a	1.2	Table 11.4-1
Maximum short period spectral response	S_{MS}	0.137	Equation 11.4-3
Spectral Response at 1 sec	S_1	0.073g	Section 11.4.1
Velocity-based site coefficient	F_v	1.7	Table 11.4-2
Maximum spectral response at 1 sec	S_{M1}	0.083g	Equation 11.4-4
Response modification factor	R	3.0	Table 12.2-1
Deflection amplification factor	C_d	3.0	Table 12.2-1
N-S building period	T	1.161 s	Calculated on ETABS
N-S Maximum building period	T_{max}	0.708 s	Section 12.8.2
E-W building period	T	1.855 s	Calculated on ETABS
E-W Maximum building period	T_{max}	1.214 s	Section 12.8.2
Long-period transition period	T_L	12 s	Figure 22-15
N-S Seismic design coefficient	C_s	0.0487	Section 12.8.1.1
E-W Seismic design coefficient	C_s	0.0284	Section 12.8.1.1
Height above ground level	h_n	57.33 ft	
Ground level base shear N-S loading	V	484.3 k	
Overturning moment N-S loading	M	19,728 ft-k	
Ground level base shear E-W loading	V	282.8 k	
Overturning moment E-W loading	M	12,068 ft-k	

Steel Framing



First Floor Framing Plan

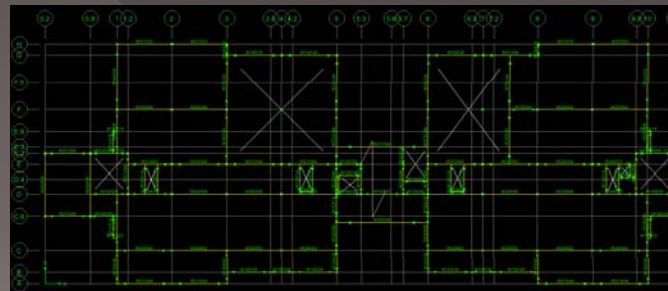
Presentation Outline

- Introduction
- Structural Depth
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 - *Proposed Redesign*
- Building Enclosures Breadth
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- Conclusions

Wind Loads

Wind Design Summary			
Design Parameter	Symbol	Value	ASCE 7-05 Reference
Occupancy category		III	Table 1.1
Wind design method		Method 2	
Wind importance factor	I	1.15	Table 6-1
Exposure category		B	Section 6.5.6.3
Enclosure classification		Enclosed	
Wind directionality factor	k_d	0.85	Section 6.5.4.4 & Table 6-4
Topographical factor	k_z	1.00	Table 6.5.7.2
Basic wind speed	V	90 mph	Figure 6-1
Approximate building period	T_b	0.438 s	Equation 12.8-7
Gust effect factor	G	0.85	Section 6.5.8
North-South length		356.25 ft	
East-West length lower 2 levels		134.0 ft	
East-West length top 2 levels		86.0 ft	
Height above grade	h_a	61.33 ft	
Ground level base shear N-S Wind	V	348 k	
Overtuning moment N-S Wind	M	13,516 ft-k	
Ground level base shear E-W Wind	V	71 k	
Overtuning moment E-W Wind	M	1175 ft-k	

Steel Framing

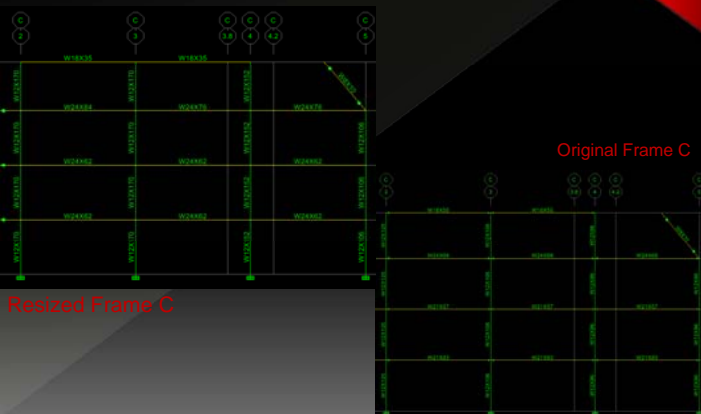


First Floor Framing Plan

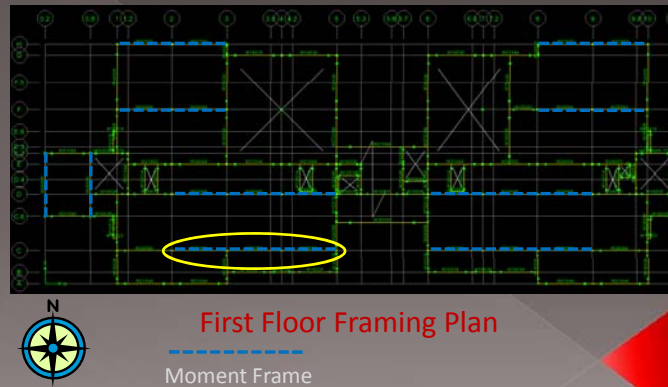
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Lateral Resisting System



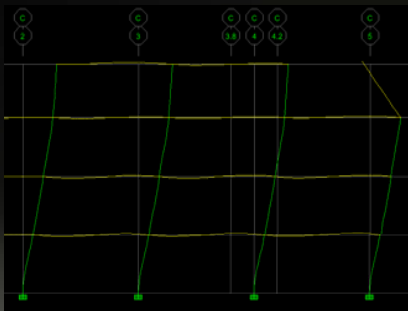
Steel Framing



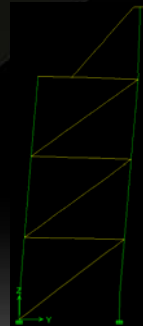
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Lateral Displacement



Moment Frame C Deflection Under Seismic Loading



Braced Frame 3 Deflection Under Seismic Loading

Story Drifts

Seismic Story Drift							
Story	Height (ft)	Deflection Amplification Factor, C_w	ETABS Displ. in E-W direction (in)	Amplified Story Drift in E-W direction (in)	ETABS Displ. in N-S direction (in)	Amplified Story Drift in N-S direction (in)	Allowable Drift = $0.015h_{ux}$ (in)
Roof	57.33	3.0	1.212	0.017	1.007	0.031	2.40
Mech.	44.00	3.0	1.205	0.835	0.994	0.737	2.64
2nd	29.33	3.0	0.857	0.998	0.687	0.929	2.64
1st	14.67	3.0	0.441	1.058	0.300	0.720	2.64

Wind Story Drift						
Story	Height (ft)	ETABS Displ. in E-W direction (in)	Story Drift in E-W direction (in)	ETABS Displ. in N-S direction (in)	Story Drift in N-S direction (in)	Allowable Drift = $h/400$ (in)
Roof	57.33	0.235	0.000	0.717	0.013	0.40
Mech.	44.00	0.235	0.052	0.704	0.217	0.44
2nd	29.33	0.183	0.078	0.487	0.263	0.44
1st	14.67	0.105	0.105	0.224	0.224	0.44

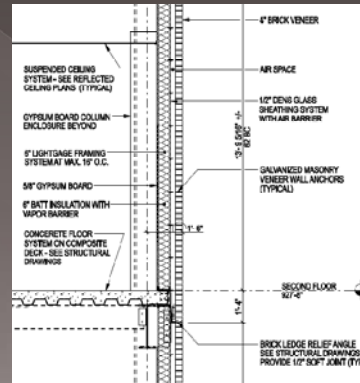
Presentation Outline

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Existing Walls



Existing Walls



Typical Wall Section

Presentation Outline

- Introduction
- Structural Depth
- Building Enclosures Breadth
 - *Existing Conditions*
 - Proposed Redesign
- Construction Management Breadth
- Conclusions



Proposed Redesign

- Goals
 - Accelerated construction schedule
 - Decrease or maintain cost
 - Minimize architectural effects
 - Retain thermal properties
- Method
 - Prefabricated wall panels
 - Precast concrete insulated sandwich panels

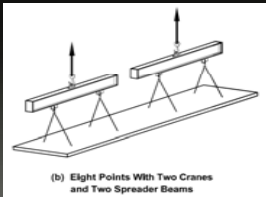
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Proposed Wall Panels



Thin Brick provides look of traditional brick veneer



(b) Eight Points With Two Cranes and Two Spreader Beams

Panel Stripping Configuration

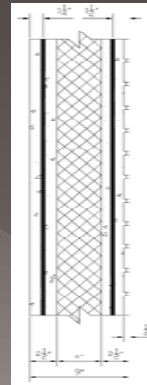


Panel Erection

Typical Sandwich Wall Panel



Typical 12' Wall Panel



Panel Cross Section

Presentation Outline

- Introduction
- Structural Depth
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 - Proposed Redesign*
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Thermal Resistance

Existing Wall					
Insulated Path					
A	Thickness	U - 1/R	R - 1/U	R - 1/U	Summation
A. Outside Surface			0.17		0.17
B. 4" Face Brick	4.0	0.25	4.00		4.17
C. 1.5" Air Gap, $\alpha_{air} = 0.16$			0.63		4.80
D. 1/2" Gypsum Sheathing			1.10		5.90
E. 2" Rigid Insulation, R-19			19.00		24.90
F. 1/2" Gypsum Sheathing			1.10		26.00
G. 1/2" Air Gap, $\alpha_{air} = 0.16$			0.63		26.63
H. Inside Surface			0.68		27.31
Total			27.31		27.31

Existing Wall					
Steel Stud Path					
A	Thickness	U - 1/R	R - 1/U	R - 1/U	Summation
A. Outside Surface			0.17		0.17
B. 4" Face Brick	4.0	0.25	4.00		4.17
C. 1.5" Air Gap, $\alpha_{air} = 0.16$			0.63		4.80
D. 1/2" Gypsum Sheathing			1.10		5.90
E. 2" Rigid Insulation, R-19			19.00		24.90
F. 1/2" Gypsum Sheathing			1.10		26.00
G. 1/2" Air Gap, $\alpha_{air} = 0.16$			0.63		26.63
H. Inside Surface			0.68		27.31
Total			27.31		27.31

Existing Wall					
Window Path					
A	Thickness	U - 1/R	R - 1/U	R - 1/U	Summation
A. Outside Surface			0.17		0.17
B. 12" Insulated Window			2.86		3.03
C. Inside Surface			0.68		3.71
Total			3.79		3.71

Typical Panel			
Area (ft ²)	% A _s	U-Value	R-Value
Gross Area	548.00		
Window Area	99.55	18.30%	
Steel Stud Area	20.83	3.81%	
Insulated Area	413.62	77.87%	
Total R-Value			
Window	11.35 R ² -ft ² -hr/Btu		4.578 Insi
Summer	11.20 R ² -ft ² -hr/Btu		6.778 Insi

Existing Wall R-Values

Sandwich Wall Panels					
Insulated Path					
A	Thickness	U - 1/R	R - 1/U	R - 1/U	Summation
A. Outside Surface			0.17		0.17
B. 1/2" Thin Brick	0.5	18.20	0.05		0.22
C. 1" AAC	2.0	5.00	0.20		0.42
D. 4" Expanded Polystyrene	4.0	0.25	4.00		4.42
E. 2.5" AAC	2.5	4.00	0.25		4.67
F. Inside Surface			0.68		5.35
Total			5.35		5.35

Sandwich Wall Panels					
Uninsulated Path					
A	Thickness	U - 1/R	R - 1/U	R - 1/U	Summation
A. Outside Surface			0.17		0.17
B. 1/2" Thin Brick	0.5	18.20	0.05		0.22
C. 0.5" AAC	0.5	2.00	0.50		0.72
D. Inside Surface			0.68		1.40
Total			1.40		1.40

Sandwich Wall Panels					
Window Path					
A	Thickness	U - 1/R	R - 1/U	R - 1/U	Summation
A. Outside Surface			0.17		0.17
B. 12" Insulated Window			2.86		3.03
C. Inside Surface			0.68		3.71
Total			3.79		3.71

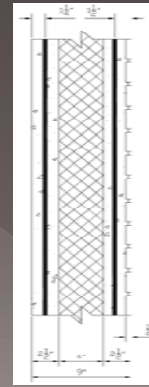
Typical Panel			
Area (ft ²)	% A _s	U-Value	R-Value
Gross Area	548.00		
Window Area	99.55	18.30%	
Uninsulated Area	8.00	1.47%	
Insulated Area	430.45	80.23%	
Total R-Value			
Window	10.61 R ² -ft ² -hr/Btu		4.578 Insi
Summer	10.44 R ² -ft ² -hr/Btu		6.778 Insi

Proposed Wall R-Values

Typical Sandwich Wall Panel



Typical 12' Wall Panel



Panel Cross Section

Presentation Outline

- Introduction
- Structural Depth
- Building Enclosures Breadth
 - Existing Conditions
 - *Proposed Redesign*
- Construction Management Breadth
- Conclusions

Existing Structure Cost

Old Structure - Composite Floor	Equivalent Square Foot Cost					Total
	Cost/SF	Floor Area (SF)				
		1st Floor	2nd Floor	Mech. Floor	Roof	
						88,298 SF
Concrete, 4000 psi, slab <6", pumped	1.54	25943	20278	19281	0	\$100,682
18g. Composite Deck, 3" deep	2.36	25943	20278	19281	0	\$154,319
20g. Wide Rib Roof Deck, 1.5" deep	2.08	0	11520	0	11276	\$47,416
WWF 6x6 W2.9xW2.9	0.38	25943	20278	19281	0	\$24,614
Finish Floor, Monolithic Screed	0.30	25943	20278	19281	0	\$19,582
Steel Beams	8.92	25943	31798	19281	11276	\$787,200
Steel Columns	4.20	25943	31798	19281	11276	\$371,150
Shear Studs, 3/4" diam., 4-7/8" long	0.16	25943	20278	19281	0	\$40,200
Total	\$17.16	\$445,173	\$347,964	\$330,855	\$0	\$1,515,163

Proposed Structure Cost

New Structure - Hollowcore Plank	Equivalent Square Foot Cost					Total
	Cost/SF	Floor Area (SF)				
		1st Floor	2nd Floor	Mech. Floor	Roof	
						88,298 SF
10" Hollowcore	7.67	25943	31798	19281	11276	\$677,266
2" Concrete Topping, 3000 psi, slab <6", pumped	0.59	25943	20278	19281	0	\$38,400
WWF 6x6 W1.4xW1.4	0.28	25943	20278	19281	0	\$18,459
Finish Floor, Monolithic Screed	0.30	25943	20278	19281	0	\$19,582
Steel Beams	4.19	25943	31798	19281	11276	\$369,707
Steel Columns	4.76	25943	31798	19281	11276	\$420,502
Shear Studs, 3/4" diam., 4-3/16" long	0.02	25943	31798	19281	11276	\$1,782
5/8" Supporting A36 Steel Plate	1.58	25943	31798	19281	11276	\$139,228
1/4" A36 Bracket Plates	0.20	25943	31798	19281	11276	\$17,631
3/16" Fillet Welds	0.22	25943	31798	19281	11276	\$44,356
Total	\$19.64	\$509,415	\$624,383	\$378,600	\$221,415	\$1,733,813

Additional Cost = \$218,650 = 14.4% Increase

If hollowcore is supported by top flange of girder, eliminates approximately \$1.83/SF, for a new total cost of \$1,572,228, only a \$57,065 increase (3.8%)

Presentation Outline

- Introduction
- Structural Depth
- Building Enclosures Breadth
- Construction Management Breadth
 - *Cost Comparison*
 - Schedule Comparison
- Conclusions

Existing Walls Cost

Old Walls - Stud Backup	Cost/SF	Wall Area (SF)			Total	
		1 Story	2 Story	3 Story		
Scaffolding - Complete System rent/mo	0.35	4184	7107	19012	30303	\$10,455
Scaffolding - labor erect/dismantle	1.14	4184	7107	19012	30303	\$34,544
16g. 6" Stl Stud Wall, 16" O.C., 16' high	2.26	4184	7107	19012	30303	\$68,527
Standard 4" Face Brick Veneer, running bond	8.13	4184	7107	19012	30303	\$246,234
3" Fiberglass Batt. Insulation, 15" wide	0.82	4184	7107	19012	30303	\$24,922
Wall Ties	0.14	4184	7107	19012	30303	\$4,274
Shelf Angles	1.63	4184	7107	19012	30303	\$49,364
Acid Brick Wash, Smooth Brick	0.52	4184	7107	19012	30303	\$15,748
Joint Backer Rod	0.09	4184	7107	19012	30303	\$2,649
Sealant	0.24	4184	7107	19012	30303	\$7,343
Flashing, Aluminum	0.36	4184	7107	19012	30303	\$11,041
Sheathing, 1/2" Dens Glass	0.90	4184	7107	19012	30303	\$27,409
Building Paper, Asphalt Felt, 15 lb.	0.17	4184	7107	19012	30303	\$5,013
5/8" Gypsum Wall Board, taped & finished	0.79	4184	7107	19012	30303	\$23,461
Total	\$17.52	573,307	\$124,538	\$333,134		\$530,981
Old Walls - CMU Backup	Cost/SF	Wall Area (SF)			Total	
Scaffolding - Complete System rent/mo	0.35	0.00	3226	0.00	3226	\$1,113
Scaffolding - labor erect/dismantle	1.14	0.00	3226	0.00	3226	\$3,678
Concrete Block Backup, Reinforced, 8" thick	0.33	0.00	3226	0.00	3226	\$1,072
Standard 4" Face Brick Veneer, running bond	8.13	0.00	3226	0.00	3226	\$26,214
1" Rigid Insulation, Perlite	0.64	0.00	3226	0.00	3226	\$2,059
Wall Ties	0.14	0.00	3226	0.00	3226	\$455
Shelf Angles	1.63	0.00	3226	0.00	3226	\$5,256
Acid Brick Wash, Smooth Brick	0.52	0.00	3226	0.00	3226	\$1,676
Joint Backer Rod	0.09	0.00	3226	0.00	3226	\$283
Sealant	0.24	0.00	3226	0.00	3226	\$782
Flashing, Aluminum	0.36	0.00	3226	0.00	3226	\$1,175
Collar Joint	0.15	0.00	3226	0.00	3226	\$488
5/8" Gypsum Wall Board, taped & finished	0.79	0.00	3226	0.00	3226	\$2,498
Total	\$14.49	50	\$46,747	50		\$577,728

Proposed Wall Panel Cost

New Walls - Sandwich Panels	Cost/SF	Wall Area (SF)				Total
		1 Story	2 Story	3 Story	Total	
9" Insulated Precast Sandwich Wall Panels with a 2.5" - 4" - 2.5" layup with 1/2" thin brick exterior	30.62	4184	10334	19012	33529	\$1,026,669
Total before 30% O&P	\$23.55					\$789,745

Cost of panel quoted by Nitterhouse Concrete Products, Inc. to be \$29.00/SF including overhead and profit, which was approximated to be 30%

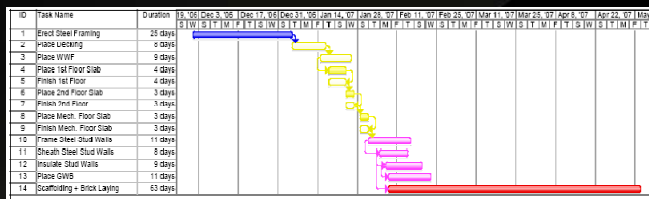
Labor cost calculated by the rate of a steel erection crew (C-11) erecting 12 panels/day

Additional Cost = \$212,017 = 36.7% Increase

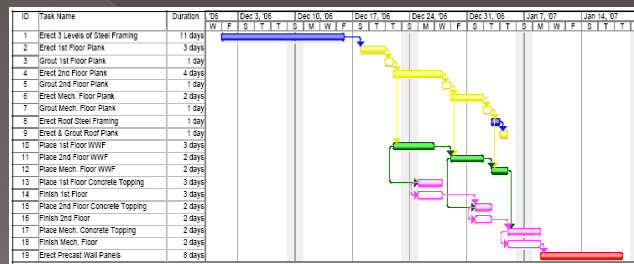
Presentation Outline

- Introduction
- Structural Depth
- Building Enclosures Breadth
- Construction Management Breadth
 - *Cost Comparison*
 - Schedule Comparison
- Conclusions

Existing Systems Schedule



Proposed Systems Schedule



Approximately 5 weeks saved from critical path
Subcontractors in the building interior sooner
Increased flexibility from addition of float time

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Further Considerations

- Project circumstances and local practices
- Impact on garage structure and foundations
- Increase structural sandwich to eliminate hollowcore supporting plates
- Fabrication lead times
- Full vibration and acoustical analysis of hollowcore planks
- Transfer beam on northern wall for wall panels
- Change of substructure to precast concrete

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Final Recommendations

- All goals met except cost control
- Current structural and wall systems best for the project
 - No time constraints so accelerated schedule not a necessity
 - No direct advantage to justify increased cost

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Acknowledgements

- My parents – Victoria and Edward Kirk
- Miami University of Ohio
- Steve Nearhoof and Alex Wing – Burt Hill
- John Jones, Bart Staley, Mike Thomas, Cliff Miles – Nitterhouse Concrete Products, Inc.
- Dr. Andres Lepage, Dr. John Messner – PSU AE
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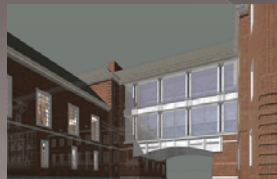
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Questions & Answers



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Wall Panel Connections



PSA Slotted Insert by JVI

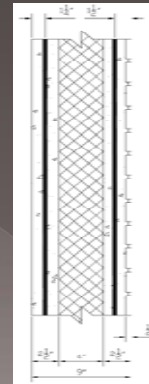


4-Way Adjustment
Connection at Column

Typical Sandwich Wall Panel



Typical 12' Wall Panel



Panel Cross Section

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Gravity Loads

Dead Loads

Item	Weight
10" Hollowcore Plank	68 psf
2" Concrete Topping (Normal Weight)	25 psf
Steel Framing	5 psf
Ceiling and Mechanical Allowance	
Typical Floor	15 psf
Mechanical Floor	25 psf
Roof	10 psf
Garage	10 psf
Partition Allowance	10 psf
Roof Materials	
4" Rigid Insulation	6 psf
Metal Deck	2 psf
Roof Membrane	1 psf
1/2" Gypsum Board	2 psf

Live Loads

Area	Design Live Load
Typical Floor	100 psf
Labs at Ground Level	125 psf
Mechanical Equipment Rooms	150 psf
Plaza	100 psf
Roof	25 psf
Parking Decks	50 psf

Proposed Redesign

- Goals and Design Constraints
 - Accelerated construction schedule
 - Decrease or maintain cost
 - Do not change architecture
 - Maintain floor-to-ceiling and total heights
- Method
 - Prefabricated structure
 - Precast concrete hollowcore floor planks
 - Supported on similar steel frame

Presentation Outline

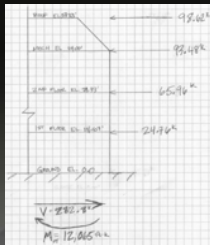
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Seismic Loads

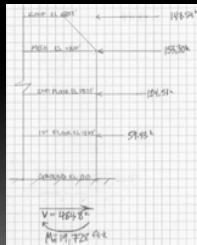
Lateral Seismic Force Distribution Through the Levels (East West Moment Frames)						
Level	Story Height	Story Weight	Exponent	$\frac{1}{h} \sum W_i h_i^2 C_{di}$	Story Force	Shear
	h_i	W_i		C_{di}	F_x	V_x
Roof	17.33 ft	1427 k	1.0771	1.260146	0.2487	98.8 k
Mech.	44.00 ft	2161 k	1.0771	1.260145	0.3267	126.8 k
2nd	26.33 ft	2627 k	1.0771	1.260145	0.2132	83.9 k
1st	14.67 ft	3512 k	1.0771	1.260145	0.0875	33.3 k
Sum		$W = 9922 k$			$V = 342.8 k$	$M = 13305 k-ft$

Lateral Seismic Force Distribution Through the Levels (North-South Braced Frames)						
Level	Story Height	Story Weight	Exponent	$\frac{1}{h} \sum W_i h_i^2 C_{di}$	Story Force	Shear
	h_i	W_i		C_{di}	F_x	V_x
Roof	17.33 ft	1427 k	1.1304	1.16835	0.3043	147.5 k
Mech.	44.00 ft	2161 k	1.1304	1.16835	0.3162	153.1 k
2nd	26.33 ft	2627 k	1.1304	1.16835	0.2168	104.5 k
1st	14.67 ft	3512 k	1.1304	1.16835	0.0726	34.7 k
Sum		$W = 9922 k$			$V = 436.8 k$	$M = 10728 k-ft$

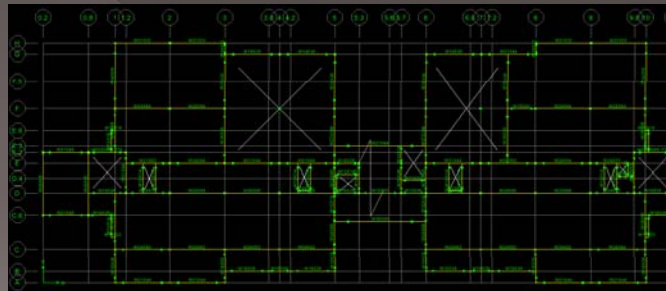
E-W Moment Frame Distribution



N-S Braced Frame Distribution



Steel Framing



First Floor Framing Plan

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